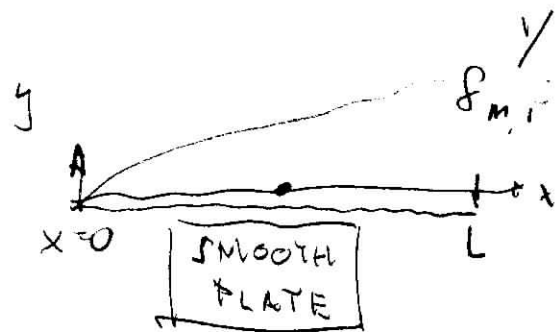


OK, so for a flat plate of length  $x$   
we found friction coef. to be



Laminar

$$S(x) = \frac{4.91x}{\sqrt{Re(x)}}$$

$$C_f(x) = \frac{0.664}{\sqrt{Re(x)}}$$

for

$$Re(x) < 5 \times 10^5$$



Turbulent

$$S(x) = \frac{0.38x}{(Re(x))^{1/5}}$$

$$C_f(x) = \frac{0.059}{(Re(x))^{1/5}}$$

for  $5 \times 10^5 \leq Re(x) \leq 10^7$



Recall:  $Re(x) = \frac{x U_\infty}{\nu}$

Note  $\lim_{x \rightarrow 0} C_f(x) \rightarrow \infty$

We can define average values as

$$\bar{f} = \frac{1}{L} \int_{x=0}^L f(x) dx$$

in which case

All  
Laminar

$$\bar{C}_f = \frac{1}{L} \int_{x=0}^L 0.664 \left( \frac{U_\infty x}{\nu} \right)^{-1/2} dx = \dots = \frac{1.328}{\sqrt{Re(L)}}$$

for  $Re(L) < 5 \times 10^5$

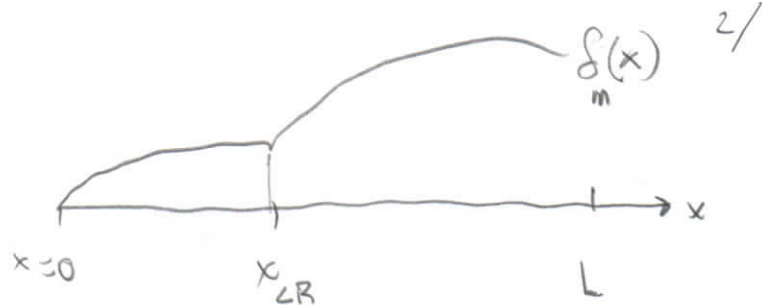
All  
Turbulent

$$\bar{C}_f = \dots = \frac{0.074}{(Re(L))^{1/5}}$$

$5 \times 10^5 \leq Re(L) \leq 10^7$

lam. & turb. conditions over the entire length  
of the plate.

But what about average values  
for laminar, then turb.?



Define

$$\bar{C}_f = \frac{1}{L} \left[ \int_{x=0}^{x_{LR}} C_f(x) dx + \int_{x=x_{LR}}^L C_f(x) dx \right] = \dots$$

laminar                      turb.

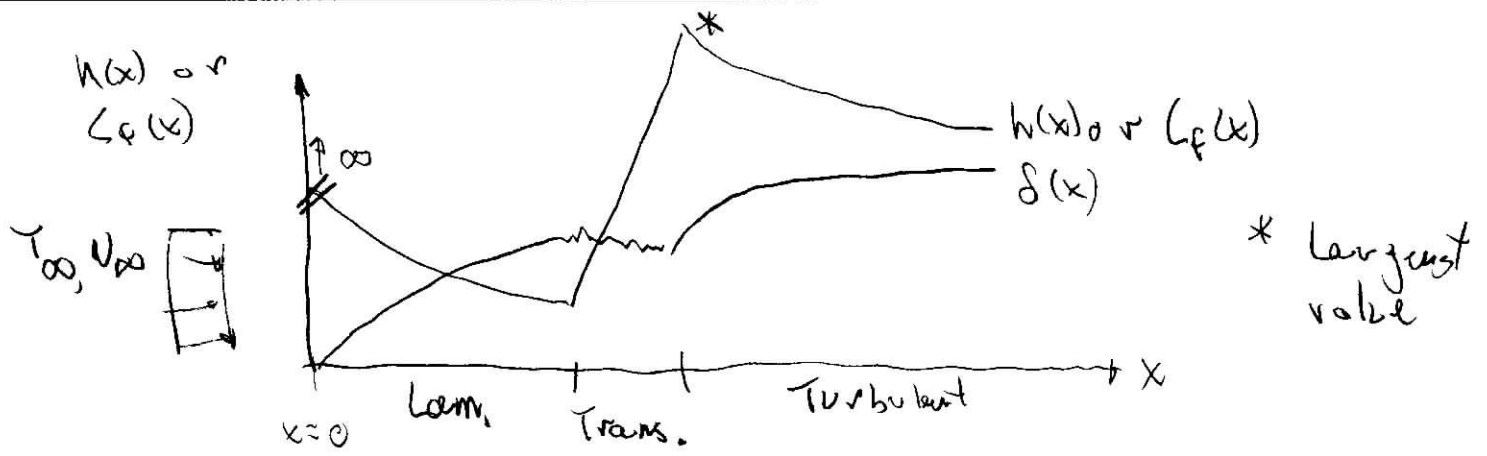
$$\bar{C}_f = \frac{0.074}{(\text{Re}(L))^{1/4}} - \frac{1742}{\text{Re}(L)} \quad 5 \cdot 10^5 \leq \text{Re}(L) \leq 10^7$$

See text for rough plates, or Hermann Schlichting (1979)

Now for heat transfer coef  $h(x)$  and Nusselt #  $Nu(x)$   
local values! We found for a smooth plate

Lam.  $Nu(x) = \frac{x h(x)}{k} = 0.332 \text{Re}(x)^{1/2} \text{Pr}^{1/3} \quad \text{Pr} > 0.6$   
 $\text{Re}(x) < 5 \cdot 10^5$

Turb.  $Nu(x) = \frac{x h(x)}{k} = 0.0296 \text{Re}(x)^{0.8} \text{Pr}^{1/3} \quad 0.6 \leq \text{Pr} \leq 60$   
 $5 \cdot 10^5 \leq \text{Re}(x) \leq 10^7$   
note:  $\lim_{x \rightarrow \infty} Nu(x) \rightarrow \infty$



The laminar  $\bar{Nu} = \frac{\bar{h} L}{k} = 0.564 Re(L)^{1/2} Pr^{1/3}$   $Pr > 0.6$   
 $Re(L) < 5 \cdot 10^5$

Turbulent  $\bar{Nu} = \frac{\bar{h} L}{k} = 0.037 Re(L)^{4/5} Pr^{1/3}$   $0.6 \leq Pr \leq 60$   
 $5 \cdot 10^5 \leq Re(L) \leq 10^7$

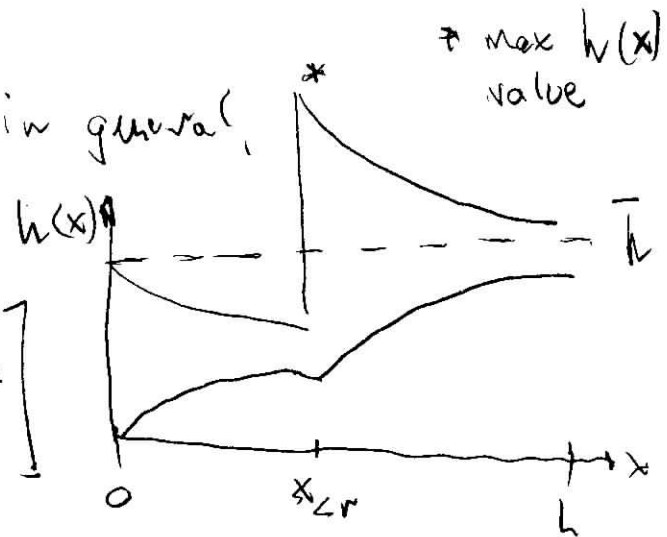
Notice that

$z(x) = \bar{z}$  in general, \* max  $h(x)$  value

For part lam. + part turb.

$$\bar{h} = \frac{1}{L} \left[ \int_{x=0}^{x_{cr}} h(x) dx + \int_{x=x_{cr}}^L h(x) dx \right]$$

lam. turb.



So  $\bar{Nu} = \frac{\bar{h} L}{k} = \left[ 0.037 Re(L)^{0.8} - 871 Pr^{1/3} \right]$   $0.6 \leq Pr \leq 60$   
 $5 \cdot 10^5 \leq Re(L) \leq 10^7$

For liquid metals  $Pr \ll 1$  (mom. diff.  $\ll$  Ther. diff.)

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$$\text{so } \delta_m \ll \delta_T$$

in which case you assume  $\approx$  constant velocity inside  $\delta_T$  of  $V_\infty$

$$\text{Then } Nu(x) \approx 0.565 (Re(x) Pr)^{\frac{1}{2}} = 0.565 Pe(x)^{\frac{1}{2}}$$

$$Pr \lesssim 0.05$$

$$Pe(x) \geq 100$$

$$Pe(x) = Re(x) Pr \quad \underline{Pe(x) \text{ of } \#}$$

---

one-size fits all (total curve fitting job!)

$$Nu(x) = \frac{h(x)x}{k} = \frac{0.3387 Pr^{\frac{1}{3}} Re(x)^{\frac{1}{2}}}{\left[1 + \left(0.0468/Pr\right)^{\frac{2}{3}}\right]^{\frac{1}{4}}}$$

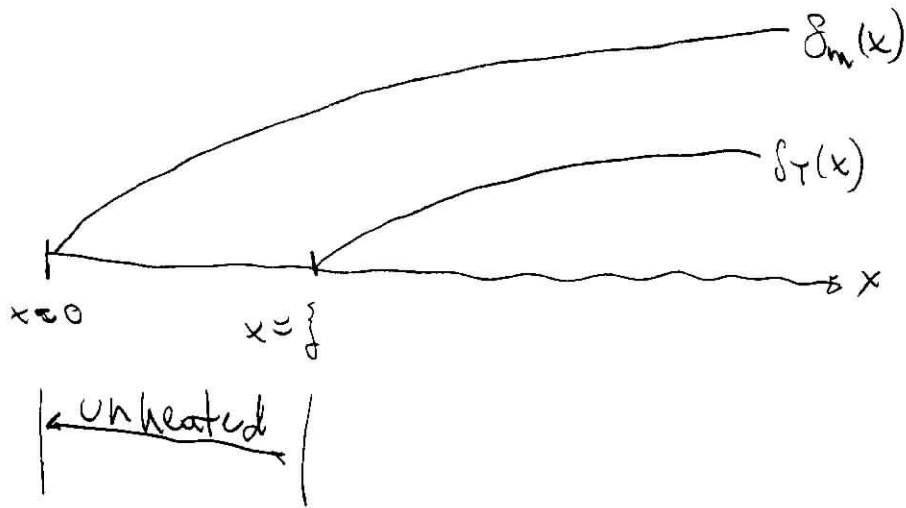
$$Re(x) Pr \geq 100$$

Good to within  $\approx \pm 1\%$  of "correct"  $Nu(x)$ .

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Unheated starting section

5/



$$\text{Laminar } Nu(x) = \frac{Nu(x)|_{\text{for } \xi=0}}{\left[1 - \left(\frac{\xi}{x}\right)^{3/4}\right]^{1/3}} = \frac{0.332 Re(x)^{1/2} Pr^{1/3}}{\left[1 - \left(\frac{\xi}{x}\right)^{3/4}\right]^{1/3}}$$

$$\text{Turb. } Nu(x) = \frac{Nu(x)|_{\text{for } \xi=0}}{\left[1 - \left(\frac{\xi}{x}\right)^{9/10}\right]^{1/9}} = \frac{0.0296 Re(x)^{0.8} Pr^{1/3}}{\left[1 - \left(\frac{\xi}{x}\right)^{9/10}\right]^{1/9}} \quad \text{if } x > \xi$$

$$\text{Laminar } \bar{h} = \frac{2 \left[1 - \left(\frac{\xi}{L}\right)^{3/4}\right]}{(1 - \xi/L)} h(L)$$

$$\text{Turb. } \bar{h} = \frac{5 \left[1 - \left(\frac{\xi}{L}\right)^{9/10}\right]}{4 (1 - \xi/L)} h(L)$$

But wait, there's more!

6/

What about uniform heat flux at the plate instead of uniform temperature?

Lam.  $Nu(x) = 0.453 Re(x)^{1/2} Pr^{1/3}$   $Pr > 0.6$   
 $Re(x) < 5 \cdot 10^5$

Turb.  $Nu(x) = 0.0308 Re(x)^{4/5} Pr^{1/3}$   $0.4 \leq Pr \leq 60$   
 $5 \cdot 10^4 \leq Re(x) \leq 10^7$

then  $q_{surf} = q''_{surf} A_{surf}$

and  $q''_{surf} = h(x) [T_s(x) - T_\infty] \Rightarrow T_s(x) = T_\infty + \frac{q''_{surf}}{h(x)}$

heat transfer surface area

Examples to follow.